**Corrections from the PhD Thesis “Building Integration of a Solar Air Heating System” requested by the examiners**

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1. The page numbers have been altered as asked. Now, pages before the Introduction, excluding the cover page, have been numbered in Roman and from Chapter 1 and so on are in Arabic, starting from 1.
2. All the text has been scanned by Grammarly and all spelling and grammar issues have been fixed throughout the whole file.
3. All variables and parameters declared for the first time have been described with their respective units for every equation.
4. The symbol list located before the Table of contents (page v) is now updated and now it includes all variables and acronyms used in the text.
5. Gair is now declared for the first time on page 76 after Eq. (1): “…where Aout is the cross-section area of the outlet pipe (m2), dair is the air density (kg/m3) and Gair is the mass airflow rate per absorber area (kg/(s.m2))”.
6. Actually, the examiner has mistakenly read aabs instead of αabs. The term refers to the absorptivity of the absorber plate. It has been declared on page 22 after Eq. (2.7).
7. Figure 5.20 on page 110 has been amended as asked.
8. The document’s formatting has been altered to avoid all unnecessary hyphenation.
9. The document’s text has been adjusted to avoid breaking paragraphs by the insertion of figures.
10. The following sentence has been added to the text on page 85: “The data were not normalized to account for these variations, which may have led to fluctuations in the observed response variables. Future studies could apply normalization techniques to improve comparison of results across different climatic conditions”.
11. The text, especially in Chapter 2 has been examined and expressions like fast, moderately have been changed or deleted without losing meaning.
12. The highlighted expression on page 21 is part of the literature review on CPCs: it means that the maximum aperture length is achieved when the reflectors’ shapes are parallel to the optical axis. This expression has been deleted from the text because there is no significant importance to the study, but only a contextualisation of concentrating collectors in general.
13. An additional expression has been inserted on page 10 to address the question: “In practice, as the air temperature approaches the absorber temperature, the heat transfer rate slows, requiring infinitely large surface areas or time to achieve the maximum possible heat transfer”.
14. The following analysis has been added, as well as Figure 4.10 on page 80: “This result can be compared to the energy distribution obtained by the ray tracing  
    algorithm used in Chapter 3 and shown in Figure 4.10. The analysis indicates that the  
    left end of the absorber surface received significantly more energy compared to the right  
    end, which is clearly reflected in the corresponding measured temperatures. In particular,  
    the higher temperatures at the left end suggest that it is more effectively absorbing energy.  
    Conversely, although the right end does not receive direct radiation, its temperatures are  
    still relatively close to the average. This suggests that some level of energy redistribution  
    or thermal conduction may be occurring. In summary, this analysis provides a means to  
    validate the previously developed optical modelling”.
15. The paragraph has been altered and referenced on page 10 as follows: “Another way to calculate the efficiency is based on the air temperature, particularly Tin and Tout at the inlet and outlet of the collector, respectively (Duffie and Beckman, 2013)”.
16. The expression “(in Heat Transfer textbooks it is also known as heat exchange effectiveness)” on page 10 has been deleted and the whole phrase has been referenced: “Eq. (2.3) can be rewritten by adding a multiplicative term known as the heat removal  
    factor or heat exchange effectiveness. It is defined as the ratio of the heat transferred to  
    the airflow to the maximum possible heat transfer if the outlet air temperature was heated  
    to the absorber surface temperature (Kutscher, 1994).”
17. The legend of Figure 3.3 on page 46 has been amended: “Solar position diagram for 53.35◦ of latitude north”.
18. The item on page 53 has been amended: “A density of 1 ray per mm2 of aperture was initially placed on the surface, with rays distributed evenly. Each ray carried equal energy, independent of the solar altitude and azimuth angles. While higher ray densities were tested, they showed no significant impact on optical efficiency and only increased computing power”.
19. Figure 4.9 has been added in Chapter 4 on page 80 as well as the following discussion: “Figure 4.9 shows the measured temperatures for each thermocouple positioned on  
    the absorber surface in order to investigate the stagnation point. The temperatures at  
    the left end (T10/T11/T12) are slightly higher than those at the right (T1/T2/T3). This  
    difference can be attributed to the fact that at 14:00 on 2nd July, the Sun’s azimuth angle  
    is 14°. Consequently, a concentration of energy may be occurring on the left side, which  
    explains the temperature variation. Another observation is that the energy flux was well  
    distributed along the area, as most temperatures are near the average value”.
20. Chapter 6 has been entirely restructured: it has a brief outline and contains “Main conclusions and key findings” and “Suggestions for future work” as topics. More text has been added.